

Effective closing time factor

Reduced free flow area in the throttle control system:

$$f_r = \frac{Q}{Q_{max}}$$

f_r reduced free flow area in the throttle control system []

Q flow coefficient []

Q_{max} max. flow coefficient []

Relative Flow:

$$Q_p = \frac{f_r}{\sqrt{p + f_r^2(1 - p)}}$$

Q_p relative Flow []

f_r reduced free flow area in the throttle control system []

p pressure parameter []

Pressure parameter:

$$p = \frac{\Delta h}{h_0}$$

p pressure parameter []

Δh theoretical pressure in the closure at full opening [m]

h_0 rated net head [m]

Theoretical pressure in the closure at full opening:

$$\Delta h = \frac{v_0^2}{2g} * (\zeta + 1)$$

Δh theoretical pressure in the closure at full opening [m]

v_0 valve speed [m/s]

g gravitational acceleration [m/s²]

ζ local loss factor for open valve []

Valve speed:

$$v_0 = \frac{Q_0}{\frac{\pi * D_0^2}{4}}$$

v_0 valve speed [m/s]

Q_0 flow [m³/s]

D_0 valve diameter [mm]

Effective closing time factor:

$$c_{ef} = \min \left[\lim_{n \rightarrow 90} \frac{0,1}{[Q_{pn} - Q_{pn+10}]} \right] > 0,125$$

c_{ef} effective closing time factor []

Q_{pn} relative flow in position n []

Flow characteristics:

The flow characteristic is the dependence of the actual flow rate on the position of the **control actuator** of the control system.

The flow characteristics of Fig.1-7 are the dependence of the actual flow rate on the position of the **valve** of the control system.

Note: The flow characteristics (depending on the valve manufacturer) that are dependent on the position of the valve must be recalculated for dependence on the position of the **actuator**. Because before the actuator may be a member (crank mechanism, ...) that is not **linear**.

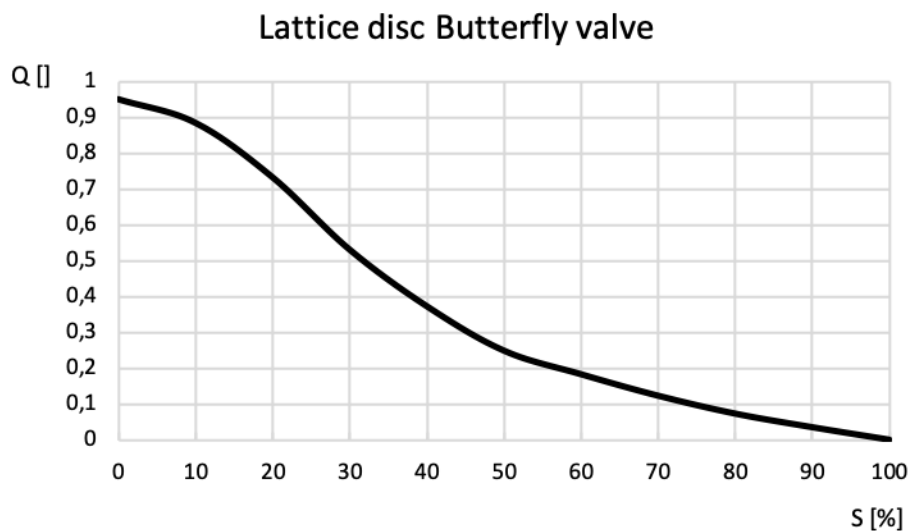


Fig.1 Flow characteristic Lattice disc Butterfly valve

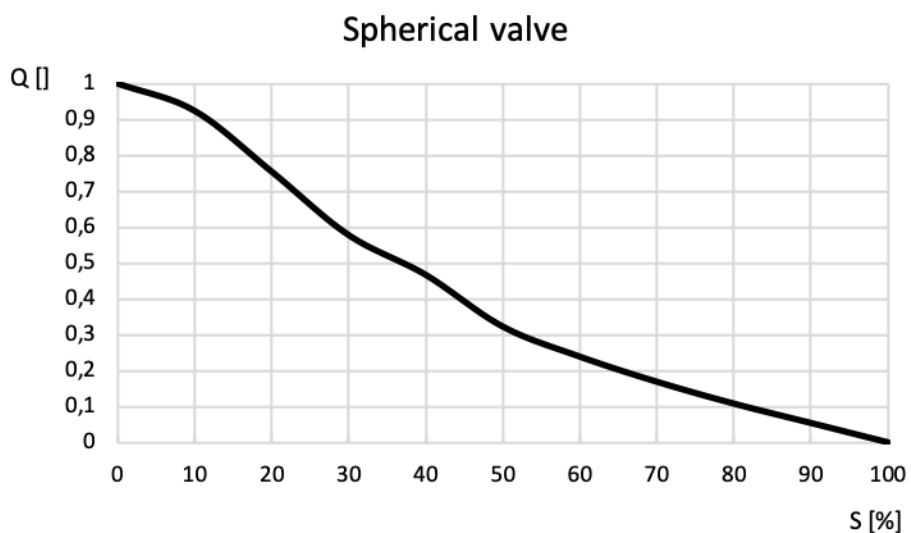


Fig.2 Flow characteristic Spherical valve

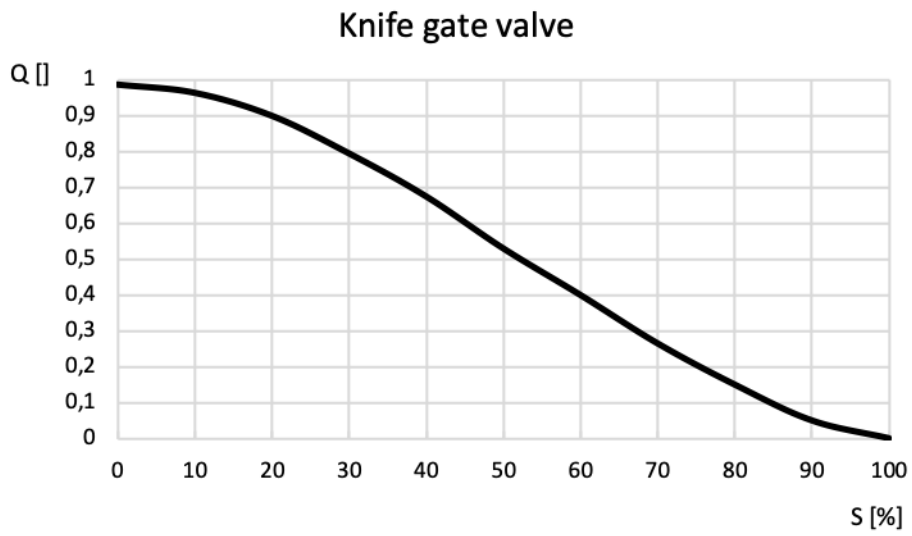


Fig.3 Flow characteristic Knife gate valve

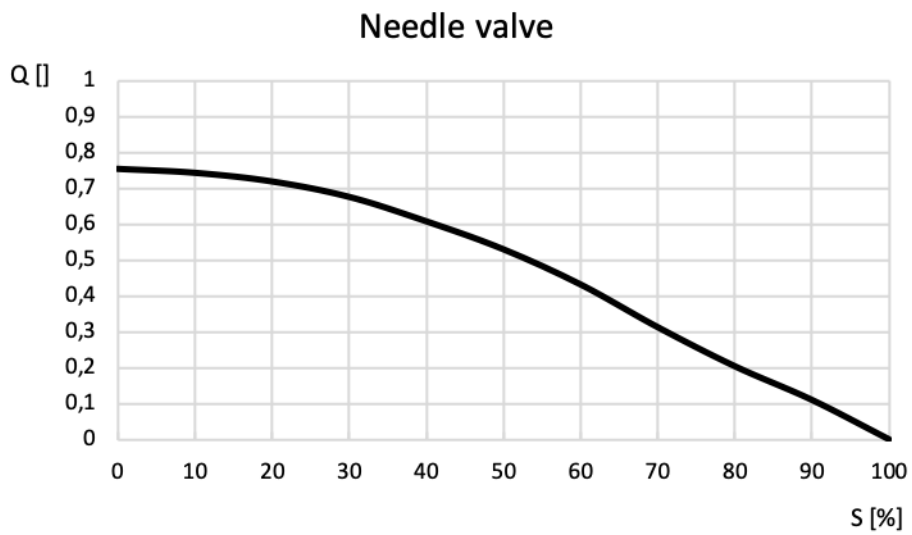


Fig.4 Flow characteristic Needle valve

Holow-Jet

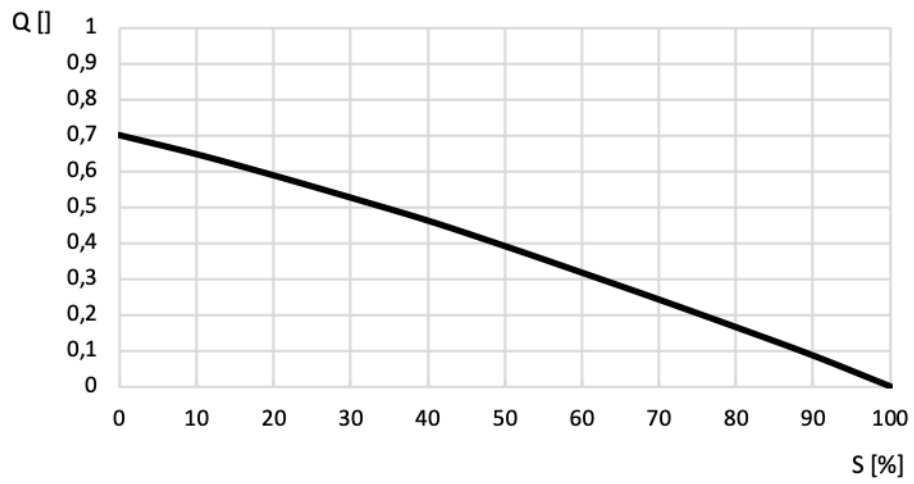


Fig.5 Flow characteristic Holow-Jet

Howell-Bunger

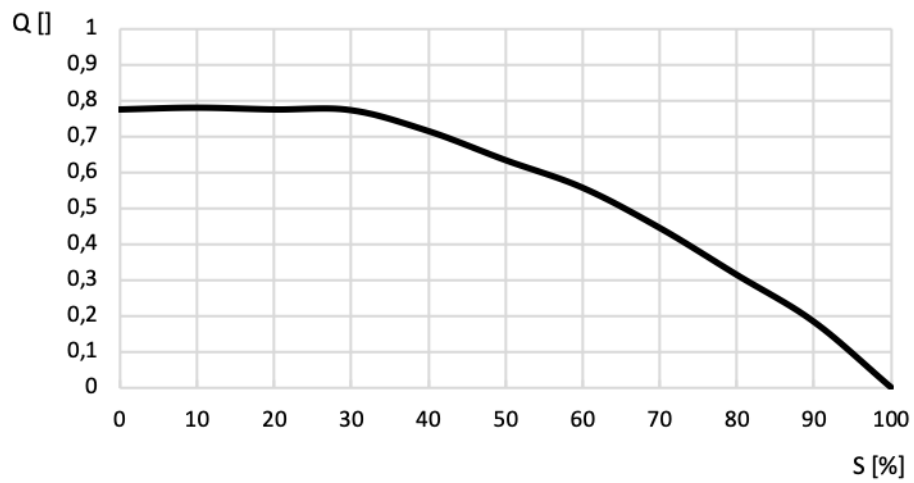


Fig.6 Flow characteristic Howell-Bunger

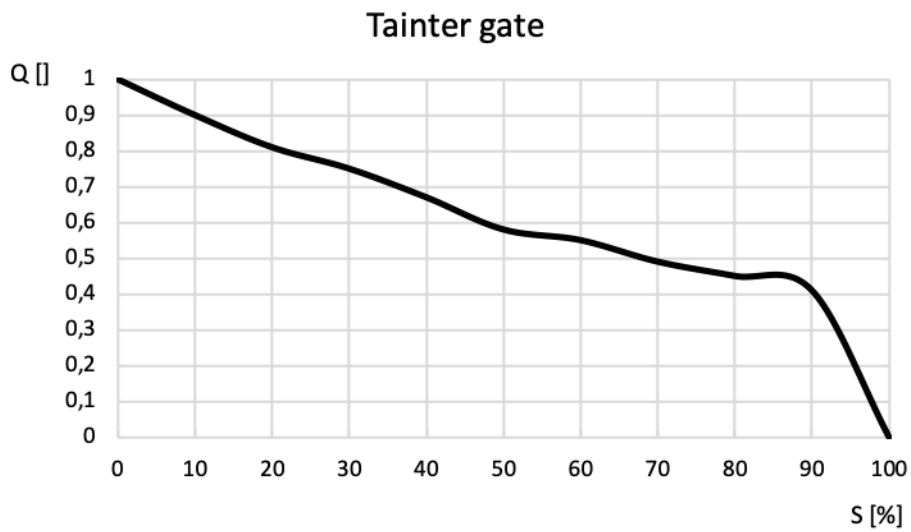


Fig.7 Flow characteristic Tainter gate

Example:

We have to determine the difference between the effective shut-off time for the flow characteristic of the valve and the flow characteristic of the control actuator (hydraulic cylinder) according to Fig.8 shut-off butterfly valve DN300 with the following parameters:
 $h_0 = 33\text{m}$; $Q_0 = 0,314 \text{ m}^3/\text{s}$; $\xi = 0,106$

	0	10	20	30	40	50	60	70	80	90	100
Q1	0,951	0,885	0,733	0,531	0,373	0,249	0,183	0,123	0,073	0,035	0,000
Q2	0,951	0,888	0,755	0,583	0,433	0,306	0,218	0,155	0,102	0,047	0,000

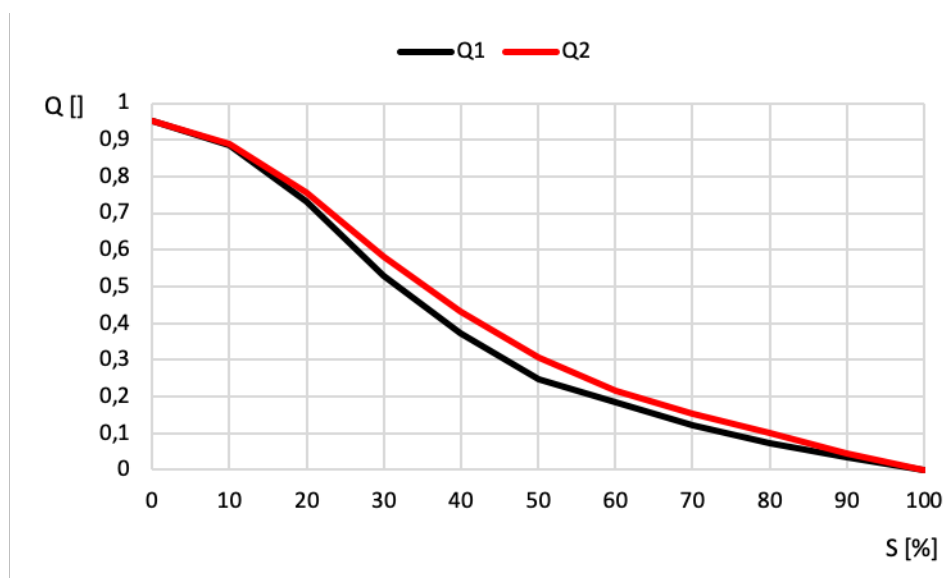


Fig.8 Flow characteristic

- Q1 flow characteristic of the valve
- Q2 flow characteristic of the control actuator

Valve speed:

$$v_0 = \frac{Q_0}{\frac{\pi * D_0^2}{4}} = \frac{0,314}{\frac{\pi * 0,3^2}{4}} = 4,44[m/s]$$

Theoretical pressure in the closure at full opening:

$$\Delta h = \frac{v_0^2}{2g} * (\xi + 1) = \frac{4,44^2}{2 * 9,81} * (0,106 + 1) = 1,11[m]$$

Pressure parameter:

$$p = \frac{\Delta h}{h_0} = \frac{1,11}{33} = 0,034[]$$

	0	10	20	30	40	50	60	70	80	90	100
Qp1	1,000	0,997	0,989	0,964	0,918	0,827	0,729	0,577	0,385	0,196	0,000
Qp2	1,000	0,998	0,990	0,973	0,941	0,879	0,787	0,667	0,505	0,259	0,000

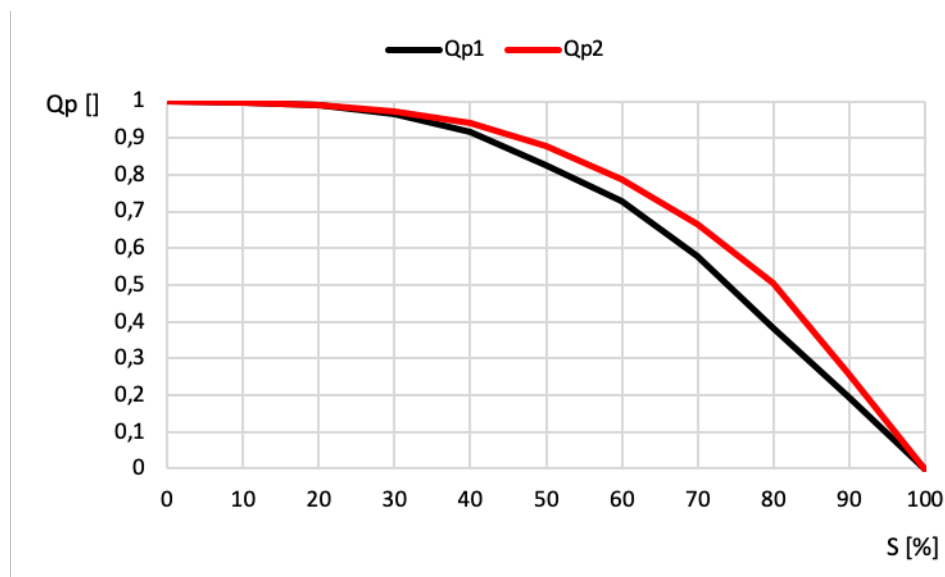


Fig.8 Relative flow characteristic $p=0,034$

Qp1 relative flow characteristic of the valve

Qp2 relative flow characteristic of the control actuator

$$c_{ef1} = 0,511[]$$

$$c_{ef2} = 0,386[]$$

c_{ef1} effective closing time factor (valve) []

c_{ef2} effective closing time factor (control actuator) []

$$x = 100 - \frac{c_{ef2}}{c_{ef1}} * 100 = 100 - \frac{0,386}{0,511} * 100 = 24,5\%$$

Literature:

F. Strohmer: Investigating the characteristics of shutoff valves by model tests. Water Power & Dam Construction 1977

By G. L. Beichley, M. ASCE and A. J. Peterka, F. ASCE: Hydraulic design of Hollow-Jet valve stilling basins. Journal of the hydraulics division 1961

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